

# **FIELD PROCEDURES FOR DETERMINING ACHIEVABLE PRECISION OF SURVEYING INSTRUMENTS: LEVELS**

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**Key words:**

## **INTRODUCTION**

The surveying profession has been subject to a rapid technical evolution concerning techniques and equipments. Today Surveyors commonly use digital levels, laserplanes, total stations and GPS however ISO (International Standard Organisation) has not yet succeeded to put on the marked standards for these new instruments. ISO still works hardly with updating and harmonisation of earlier standards for older instruments as example EDM, theodolites and levels.

Inside ISO, several Technical Commissions (TC59/SC4 and TC172/SC6) have produced standards for levelling instruments. Unfortunately these standards (ISO 8322, ISO 12857, etc) made for the same instrument and for the same purpose namely "Field procedures for determining the accuracy of surveying instruments" are often quite different because of different goals for the TC's. TC59 looked from the building construction views and TC172 from the instrument manufacturer view.

Since 1997 a Joint Working-Group for both TC's works on a harmonisation and updating of existing standards. The goal is one standard for one instrument type.

## **THE FIG STANDARDISATION ACTIVITIES**

Inside FIG (International Federation of Surveyors) it is Commission 5 who had the responsibility on questions related to survey instruments and methods. Before 1990 FIG was not much interested in ISO standards. The complexity, diversity and multitude of standards and the special ISO-language made it very difficult for the common FIG member to understand and apply these standards. Often these standards complicated the surveyor life because of the difficulty to be used under "field conditions" and therefore they were neglected.

In a first attempt to simplify and clarify the situation about EDM standards, FIG Commission 5 published 1994 at the Melbourne Congress "*Recommended procedures for routine checks of Electro-optical distance meters*". This document, easy to understand and to apply, was acceptable for the common FIG surveyor, has reached a great success inside the profession and has been translated in several languages.

After this success FIG-C5 proposed 1998 at the Congress in Brighton that guidelines for other survey instruments (levels, total stations, GPS, etc) were made until 2002.

FIG realised later one, after that EU (European Union) introduced its one CEN (Comité Européen de Normalisation) standards who are not only recommendations but laws regulating professional activities, the increasing importance of it and established 1997 a special Task Force on Standards to co-ordinate the standardisation activities inside FIG and with ISO. FIG is today also hardly involved in the activities of ISO TC 211. Several reports at this FIG C5 workshop will refer to the ISO and FIG activities on the common subjects.

After some years of collaboration FIG obtained 1999 the Class A liaison status to ISO/TC 172 SC6 and TC59. Today several members from FIG-WG 5.1 are directly engaged in the work of ISO/TC 172 SC6 on the establishment of new standards. One of the projects concerns levels and is chaired by J-M Becker. A reviewed draft proposal has been discussed in Berlin March 1999 and sends to the national standard organisations for comment and approval. This standard will probably be finalised and published at the end of this year.

The following paper present firstly general and specific surveyor requests on standards, thereafter the recommended field procedures for the determination of the *achievable precision* with levelling instruments for different applications. Simplified and a full test procedures will be shortly described. For more details we recommend to read the incoming ISO standards.

## **OBJECTIVE OF THE STANDARDS**

The objective for the standards is to specify *field procedures* to be followed each time the achievable precision or “accuracy” for a given surveying instrument used together with its ancillary equipment (tripod, staffs, etc) has to be determined. This will allow the surveyor to investigate that the precision given by the measuring equipment is appropriate to the intended-measuring task.

## **FIG REQUESTS ON STANDARDS**

The common requests are as follow:

- only *one standard for each type of instrument* (including its ancillary equipment)
- who can be used *anywhere* and
- *whiteout* any *special* ancillary equipment (like instrument of higher order or collimator, etc)
- by *common field operators* (technicians as well as academics).

That is to eliminate confusions, difficulties in applications and in interpretations.

Before any fieldwork the surveyor has to answer to the following question:

*“Can I achieve the required precision (“accuracy”) in the project with my equipment, yes or no?”*

The answer depends from the components of *each survey team* involved (instruments, ancillary equipment’s, personal), execution times, project specificity’s, environmental conditions (meteorology, vegetation, groundsurface), etc. It is the complete *survey system* who is intended to be used who has to be checked.



The question can also be more general concerning several teams, equipment's, projects, times, etc.

The Surveyor has to be convinced that if he apply the standards it will help him, otherwise he will not apply them. For these reasons the surveyor require *user friendly standards*, low time consuming for implementation (about ½ hour) (low-costs) with results easy to be interpreted.

## **FIELD PROCEDURES**

In general we follow the approach presented by FIG (1994) for EDM in several steps:

Step 1: Deliverance checks of the instrument and its ancillary (at the reception)

Step 2: Calibration (done in laboratory especially for the staffs and at regular time intervals)

Step 3: Functionality test before each specific project: see proposed procedures

The two described procedures are designed for *field* and not for laboratory use. The results are specific for *each* determination and *representative only* for the *particular conditions* existing at that *time*: weather, environment, ground surface, equipment, staff members, etc. The equipment must always be acclimated to the environmental temperature and *adjusted before testing* in accordance with the manufacturer handbooks. (Step 3).

### **Simplified field test**

This test is based on a limited number of measurements (minimum 10) for check of the levelling equipment used especially on construction *workside where radial/polar measurements with unequal sight lengths* at each set-up are normal. Equal sight lengths are exceptions.

Establishment of a test line:

In a relatively plane area two points A & B have to be monumented at a distance corresponding to the maximum and minimum sight length ranges that will be used inside each specific project. As example if the needed sight lengths inside a construction



each pair of readings *a new instrumental set-up* has to be made. All details about how to operate, calculate and evaluate are described in the coming standard with one example in appendix.

Evaluation of the results:

The results analyse is made with statistical tests helping the surveyor to decide if its equipment “yes or no” allow him to achieve the required “accuracy”.

## **CONCLUSION**

FIG-C5 is grateful that the ISO Technical Committees TC59 and TC172 have taken in account the requests from the surveyor community for the updating and harmonisation of existing standards. We also appreciate the efforts undertaken to prepare standards for the *new generation* of survey instruments like total stations, laserplanes and perhaps GPS. We hope that these standards will soon be reality.

FIG Commission 5 will contribute with its experts (WG 5,1) to the elaboration of this standards through its collaboration with ISO and the participation in the work. Furthermore FIG-C5 will help the surveyors to implement these standards in the best way.

## **CONTACT**

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## **BIOGRAPHICAL NOTE**

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# ANNEX 1

## 1 - EXAMPLE FOR SIMPLIFIED TEST METHOD

(All observations are in metres, calculations in mm)

**Instrument No:**  
2730  
Staff A A  
10AA

**Type:**  
NA 3003  
Staff B  
No:10B

**Operator:**  
HR

**Date: 2001-01-10**

**Weather: Sunny, -5 C**

| Backward= 30 m Forward= 30 m |                     |                |                |             |        | Backward= 10 m Forward= 50 m |                |                |               |       |        |
|------------------------------|---------------------|----------------|----------------|-------------|--------|------------------------------|----------------|----------------|---------------|-------|--------|
| 1 (12)                       | 2                   | 3              | 4              | 5           | 6      | 7                            | 8              | 9              | 10            | 11    |        |
| Set Up No                    | Backw<br>ard<br>rbn | Forward<br>ran | dn=<br>rbn-ran | v=<br>(x)-d | v*v    | Backward<br>rdn              | Forward<br>rcn | d'=<br>rdn-rcn | v'=<br>d'-(x) | v'*v' |        |
|                              | m                   | m              | mm             | mm          | mm2    | m                            | m              | mm             | mm            | mm2   |        |
| 1                            | 11                  | 1,6978         | 1,551          | 146,80      | -0,13  | 0,0169                       | 1,4737         | 1,3263         | 147,40        | 0,73  | 0,5329 |
| 2                            | 12                  | 1,6952         | 1,5486         | 146,60      | 0,07   | 0,0049                       | 1,4711         | 1,3235         | 147,60        | 0,93  | 0,8649 |
| 3                            | 13                  | 1,6972         | 1,5506         | 146,60      | 0,07   | 0,0049                       | 1,4824         | 1,3351         | 147,30        | 0,63  | 0,3969 |
| 4                            | 14                  | 1,6957         | 1,549          | 146,70      | -0,03  | 0,0009                       | 1,4837         | 1,3366         | 147,10        | 0,43  | 0,1849 |
| 5                            | 15                  | 1,6988         | 1,5521         | 146,70      | -0,03  | 0,0009                       | 1,4894         | 1,3427         | 146,70        | 0,03  | 0,0009 |
| 6                            | 16                  | 1,6958         | 1,5492         | 146,60      | 0,07   | 0,0049                       | 1,4937         | 1,3471         | 146,60        | -0,07 | 0,0049 |
| 7                            | 17                  | 1,6998         | 1,5531         | 146,70      | -0,03  | 0,0009                       | 1,4982         | 1,3509         | 147,30        | 0,63  | 0,3969 |
| 8                            | 18                  | .              | .              | .           | .      | .                            | .              | .              | .             | .     |        |
| 9                            | 19                  | .              | .              | .           | .      | .                            | .              | .              | .             | .     |        |
| 10                           | 20                  | 1,7041         | 1,5574         | 146,70      | -0,03  | 0,0009                       | 1,4948         | 1,3469         | 146,90        | 0,23  | 0,0529 |
| Sum(S)=                      |                     |                | 1466,7         | Sum(v*v)    | 0,0410 | Sum(S')=                     |                | 1470,60        | Sum(v'*v')    | 2,584 |        |
| Mean=                        |                     |                | 146,67         | s=          | 0,0675 | Mean=                        |                | 147,06         | s'=           | 0,508 |        |

### Calculation and Results

The arithmetic mean of the differences from (2) – (3) with equal sighting lengths give us the true value of the height difference between points A and B:  $\Rightarrow dH1 = 146,67 \text{ mm}$

The arithmetic mean from the differences (7) – (8) correspond to the height difference with maximal inequality in sight length 10 and 50 meters. This value dH2 is = 147.06 mm

The control by sums from column (5) and (10) gives zero

The difference between dH1 – dH2 = 146, 67 - 147, 06 mm = -0, 39 mm

This difference (-0,39mm) is bigger than  $2,5s = 2,5 \times 0,068 = 0, 17\text{mm}$  and the conclusion is that this value is too large. The precision of the level (equipment) is not within the permissible error limits. In this case we have firstly to check the collimation error according the user manual and thereafter probably to reduce the maximum sight length or to work with more equal sight lengths..

## ANNEX 2

### 2 -Full test method

Instrument No: 2739  
 Staff A No: 10A  
 Type: NA3003  
 Staff B: 10B  
 Operator: HB  
 Date: 28 Nov, 1997  
 Weather: Sunny, - 5 C  
 NLS

| Set Back.=30 m For.=30 m |             |             |                |              |       | Set 2 B=27 m F=33 |             |                |               |        | Set 3 B=45 m F=50 |             |                 |                 |         |
|--------------------------|-------------|-------------|----------------|--------------|-------|-------------------|-------------|----------------|---------------|--------|-------------------|-------------|-----------------|-----------------|---------|
| 1                        | 2           | 3           | 4              | 5            | 6     | 7                 | 8           | 9              | 10            | 11     | 12                | 13          | 14              | 15              | 16      |
| Set<br>Trn<br>No         | Back<br>rbn | For.<br>ran | dn=<br>rbn-ran | v=<br>(x)-dn | v*v   | Back<br>rdn       | For.<br>rcn | d'=<br>rdn-rcn | v'=<br>d'-(x) | v'*v'  | Back<br>rfn       | For.<br>ren | d''=<br>rfn-ren | v''=<br>d''-(x) | v''*v'' |
|                          | m           | m           | mm             | mm           | mm2   | m                 | m           | mm             | mm            | mm2    | m                 | m           | mm              | mm              | mm2     |
| 1                        | 1,5157      | 1,2978      | 217,9          | 0,060        | 0,004 | 1,6105            | 1,3928      | 217,7          | -0,2600       | 0,0676 | 1,3893            | 1,1710      | 218,3           | 0,340           | 0,116   |
| 2                        | 1,5166      | 1,2986      | 218,0          | -0,040       | 0,002 | 1,6143            | 1,3967      | 217,6          | -0,3600       | 0,1296 | 1,3895            | 1,1711      | 218,4           | 0,440           | 0,194   |
| 3                        | 1,5275      | 1,3093      | 218,2          | -0,240       | 0,058 | 1,6151            | 1,3973      | 217,8          | -0,1600       | 0,0256 | 1,3833            | 1,1649      | 218,4           | 0,440           | 0,194   |
| 4                        | 1,5273      | 1,3092      | 218,1          | -0,140       | 0,020 | 1,6158            | 1,3982      | 217,6          | -0,3600       | 0,1296 | 1,3885            | 1,1705      | 218,0           | 0,040           | 0,002   |
| 5                        | 1,5303      | 1,3125      | 217,8          | 0,160        | 0,026 | 1,6144            | 1,3966      | 217,8          | -0,1600       | 0,0256 | 1,3917            | 1,1739      | 217,8           | -0,160          | 0,026   |
| 6                        | 1,5401      | 1,3223      | 217,8          | 0,160        | 0,026 | 1,6150            | 1,3969      | 218,1          | 0,1400        | 0,0196 | 1,3943            | 1,1763      | 218,0           | 0,040           | 0,002   |
| 7                        | 1,5431      | 1,3249      | 218,2          | -0,240       | 0,058 | 1,6106            | 1,3928      | 217,8          | -0,1600       | 0,0256 | 1,4029            | 1,1848      | 218,1           | 0,140           | 0,020   |
| 8                        | 1,5476      | 1,3298      | 217,8          | 0,160        | 0,026 | 1,6129            | 1,3949      | 218,0          | 0,0400        | 0,0016 | 1,4036            | 1,1855      | 218,1           | 0,140           | 0,020   |
| 9                        | 1,5399      | 1,3222      | 217,7          | 0,260        | 0,068 | 1,6089            | 1,3910      | 217,9          | -0,0600       | 0,0036 | 1,4074            | 1,1892      | 218,2           | 0,240           | 0,058   |
| 10                       | 1,5327      | 1,3146      | 218,1          | -0,140       | 0,020 | 1,6119            | 1,3938      | 218,1          | 0,1400        | 0,0196 | 1,4085            | 1,1903      | 218,2           | 0,240           | 0,058   |
| 11                       | 1,4957      | 1,2779      | 217,8          | 0,160        | 0,026 | 1,6061            | 1,3883      | 217,8          | -0,1600       | 0,0256 | 1,4092            | 1,1911      | 218,1           | 0,140           | 0,020   |
| 12                       | 1,5037      | 1,2857      | 218,0          | -0,040       | 0,002 | 1,6013            | 1,3834      | 217,9          | -0,0600       | 0,0036 | 1,4163            | 1,1983      | 218,0           | 0,040           | 0,002   |
| .....                    | .....       | .....       | .....          | .....        | ..... | .....             | .....       | .....          | .....         | .....  | .....             | .....       | .....           | .....           | .....   |
| .....                    | .....       | .....       | .....          | .....        | ..... | .....             | .....       | .....          | .....         | .....  | .....             | .....       | .....           | .....           | .....   |
| 20                       | 1,4988      | 1,2809      | 217,9          | 0,060        | 0,004 | 1,6046            | 1,3868      | 217,8          | -0,1600       | 0,0256 | 1,4116            | 1,1935      | 218,1           | 0,140           | 0,020   |
|                          | Sum=        | 4359.2      | v.v=           | 0,538        |       | Sum=              | 4356.7      | v'.v'=         | 0,738         |        | Sum '=            | 4363,2      | v''.v''=        | 1,383           |         |
|                          | Mean=       | 217,96      | s=             | 0,168        |       | Mean=             | 217,84      | s'=            | 0,192         |        | Mean=             | 218.16      | s''=            | 0,263           |         |

### Calculations and Results from full test method

In this table we made the following measurements with each 20 set-ups:

- Firstly with equal sight lengths of 30 meters Backward and Forward
- Secondly unequal sight lengths within a variation of 10% around 30 m: 27 and 33m
- Thirdly we choose an application with longer distances around 50m: 45 and 50m

The results are as follow:

The arithmetic mean from the first set of measurements with equal distances (30m & 30m) is  $dH1 = 217,96 \text{ mm}$  this value can also be considered as the true value of the height difference between A and B

The arithmetic mean from the second set of measurements (27m & 33m) is  $dH2 = 217.83 \text{ mm}$

The arithmetic mean from the third set (45m & 50m) is  $dH3 = 218.16 \text{ mm}$

The sums of (5), (10) and (15) are equal to zero

The differences between  $dH1$ ,  $dH2$  and  $dH3$  are less than  $< 0.33 \text{ mm}$ .

The experimental standard deviation for the two first sets each of 20 measurements (around 30 m) is equal to:

$$S_{1,2} = \sqrt{(0.538 + 0.739) / 38} = 0.183 \text{ mm where 38 is the degree of freedom}$$

From this value the experimental standard deviation for 1-km double-run levelling can be calculated

$$S_{1,2} \text{ (1km double run)} = S_{1,2} / \sqrt{2} \times \sqrt{(1000\text{m}/60\text{m})} \text{ or } S_{1,2} \times 2.89 \text{ in our specific case we will be}$$

$$S_{1,2} \text{ (1km double run)} = 0.183 \times 2.89\text{mm} \Rightarrow \underline{0.529 \text{ mm}}$$

The second calculation is using set one and set tree

$$S_{1,3} = \sqrt{(0.538 + 1.383)/38} = 0,225 \text{ mm with 38 degree of freedom}$$

$$S_{1,3} \text{ (for 1km double run)} = 0,225 \times 2.89 = \underline{0,650 \text{ mm}}$$

Conclusion: in both cases the experimental standard deviations are smaller than the value  $\sigma$  stated by the manufacturer (<1mm) and required for our specific project.